# A Methodology for Determining Internal Stresses in Multi-Component Materials

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#### Internal stresses: Why do we care?

- Constitutive performance of structural materials
  - Operating environment and conditions
- Composites
  - Residual stresses in virgin materials
  - Both macro and micro residual/internal stresses

# Determine a safe operating space



#### Neutron diffraction

- In-situ measure internal *elastic* strains in bulk material
  - Spatially resolved
  - Changes due to applied "load":
    - Stress, Strain, Temperature, Environment...





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- ±250 kN loading capability
- Measure // and  $\perp$  strains simultaneously
- 1500 kg translator table
- RT to 1500°C vacuum furnace (1800°C stand-alone)
- RT to -100°C vacuum cryo-stage



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## **Finite Element Modeling**

- Uniaxial fiber model
- Unit-cell model
  - Hexagonal fiber stacking
- Full 3D due to loading along fibers
- Plane strain assumption
  - Plane perpendicular to fibers stay plane
- 2<sup>nd</sup> order brick elements







- Kanthal has good high temperature properties
  - Inherent corrosion/oxidization protection by forming an alumina case
  - 73.2% Fe, 21.0% Cr, 5.8% Al and 0.04%C
- Tungsten fibers increases strength
- Manufacture technique
  - Plasma sprayed
  - Mixed cubic and hexagonal stacking observed

10%







2280

- Stress-free temperature assumed to be 650°C
  - Processed at 1065°C
  - 0.7-0.8\*T<sub>P</sub>
- Material parameters
  - "Bilinear elastic-plastic"

| Temperature<br>(°C) | Young's<br>modulus<br>(GPa) | Poisson's<br>ratio | Yield<br>stress<br>(MPa) | Coefficient of thermal expansion $(10^{-6} \text{ K}^{-1})$ |
|---------------------|-----------------------------|--------------------|--------------------------|---|
| 26                  | 395                         | 0.28               | 1305                     | 4.40  |
| 138                 | 394                         | 0.28               | 1179                     | 4.42  |
| 251                 | 393                         | 0.28               | 1054                     | 4.44  |
| 420                 | 389                         | 0.28               | 893                      | 4.47  |
| 533                 | 386                         | 0.28               | 777                      | 4.49  |
| 1000                | 360                         | 0.28               | 550                      | 4.56  |

P. Rangaswamy *et al.* Table 1. Tungsten fibre thermomechanical properties used in the models.

| Table 2. | Kanthal: | thermomechanical | properties | used in | the | models. |
|----------|----------|------------------|------------|---------|-----|---------|
|----------|----------|------------------|------------|---------|-----|---------|

| Temperature<br>(°C) | Young's<br>modulus<br>(GPa) | Poisson's<br>ratio | Yield<br>stress<br>(MPa) | Coefficient of thermal expansion $(10^{-6} \mathrm{K}^{-1})$ |
|---------------------|-----------------------------|--------------------|--------------------------|--|
| 26                  | 202                         | 0.28               | 530                      | 9.58   |
| 138                 | 196                         | 0.28               | 520                      | 9.68   |
| 251                 | 183                         | 0.28               | 465                      | 10.08  |
| 420                 | 172                         | 0.28               | 375                      | 10.80  |
| 533                 | 162                         | 0.28               | 275                      | 11.38  |
| 1000                | 125                         | 0.28               | 27                       | 14.75  |



Rangaswamy et al., Phil Mag. 2003



Thermal residual strains in Kanthal/Tungsten composites

- Thermal residual strains measured and predicted
  - Large discrepancy for the matrix in the 70% composite
    - Increased yield strength due to grain refinement?
  - Transverse strains

nos

Very heterogeneous elastic strain distribution



- In-situ loading strains measured and predicted
  - Only yield region of 10% composite is outside error bars (±100με)
- Baseline for materials with well known properties
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#### Conclusions

- Thermal residual strains
  - Results for Kanthal (plastically deforming phase) inaccurate at high fiber volume fraction (70%)
  - Transverse strains are highly non-uniform and the agreement between model and measurements is not as good
- In-situ loading strains
  - The modeling approach is capable of predicting the loading behavior taking into account the thermal residual strains
  - Caveat: Very small plastic region. Only one phase deforming plastically. Only about 0.3% macroscopic plastic strain



- Bulk Metallic Glass matrix (Vitreloy 1)
  - High yield stress, low stiffness (high elastic limit)
  - Limited ductility due to shear banding
- Composites were cast in Stainless steel tubes





Thermal residual strains in BMG/Tungsten composites

- Thermal residual strains measured and predicted
  - Best agreement longitudinal
  - Uniformity of strains in the longitudinal direction
  - No plastic deformation predicted during cooling



In-situ loading strains

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Elastic strains in Tungsten only

Blue line: FEM with literature data

Red line: FEM with refined material parameters



- Macroscopic loading curves
  - Flat parts are constant load holds for the neutron diffraction measurements
- Blue line: FEM with literature data

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Red line: FEM with refined material parameters

- Conclusions
  - Method suggest that the properties of the Tungsten fibers have changed
    - Less hardening
    - More ductility
  - Some ductility in BMG is necessary to give good agreement with measured data





### SMARTS Expert

- Implement automated modeling of load sharing and phase stresses in composites using FEM
- Implement automated modeling of single crystal elastic constants using SCM



- Combined measurement and modeling scheme to determine in-situ material properties
  - Successfully tested for Kanthal/Tungsten composites
  - Suggest changes in material parameters for BMG/Tungsten composites

