Load Sharing in Tungsten Continuous Fiber Reinforced Kanthal MMC's

B. Clausen[†], M.A.M. Bourke[‡] and E. Üstündag[†]

[†]Materials Science, California Institute of Technology [‡]MST-8, Los Alamos National Laboratory





Outline

- Tungsten Continuous Fiber Reinforced Kanthal Metal Matrix Composites
- Neutron Diffraction
- Finite Element Modeling
- Self-consistent Modeling
- Conclusions



Metal Matrix Composites (MMC)



- Thermal Residual Stresses (TRS)
 - Influence mechanical behavior



Tungsten Continuous Fiber Reinforced Kanthal MMC







20%



- Kanthal has good high temperature properties
 - Inherent corrosion/oxidization protection by forming
 an alumina case
 - 73.2% Fe, 21.0% Cr, 5.8% Al and 0.04%C
- Tungsten fibers increase creep resistance
- Samples
 - Monolithic Kanthal.
 - Reference sample. No TRS.
 - 10, 20 and 30 volume percent Tungsten fibers
 - Various levels of TRS due to the differences in CTE
 - Different yield points in tension due to the TRS
- Manufacture technique
 - Arc-sprayed, NASA Lewis, Tufts University
 - Mixed cubic and hexagonal stacking observed



 λ = 2dsin θ

• TOF technique: Measure diffracted intensity as function of time-of-flight



- Differences in lattice spacing => Elastic Lattice Strain
- Unique method to non-destructively determine internal strains in bulk samples
- Phase specific measurements ideal for composites





- Neutron Powder Diffractometer (NPD) at LANSCE
- Schematic set-up for *in-situ* loading measurements
- Measurement time is about 2-4 hours per load level
- Measure elastic strains in two directions simultaneously







- The NPD load frame
 - 48 kN maximum load in tension or compression
 - Mirror furnace, 350°C maximum temperature



SMARTS: Spectrometer for Materials Research at Temperature and Stress









- SMARTS; First neutrons by May 2001
 - Order of magnitude lower count times than NPD (10-20 min)
 - 1 cubic millimeter gauge volume
 - **Combined** ±250kN, 1500°C and translation/rotation





• Rietveld refinement provides an empirical lattice elastic mean phase (LEMP) strain





- Measured macroscopic stress/strain curves
- 10 and 20% N/A due to extensometer problems
- Difference in curves?
- Young's modulus?
- Yield point?





- Measured LEMP strains
 - Monolithic Kanthal. The LEMP strain is not linear in the plastic region due to build-up of intergranular strains.
 - 10%. Co-deformation until 200 MPa. Load sharing as Kanthal becomes plastic.
 - 20%. Co-deformation until 100 MPa.
 - 30%. Region with co-deformation is very limited (about 50 MPa).
- Initial stiffness; Appears to be the same in all samples
 - Elastic region ?
- Neutron diffraction is the only tool that can provide us with this type of data



Finite Element Modeling (FEM)



FE Model for 30 volume percent Tungsten fibers

- 3D model to accommodate the "out-of-plane" loading
- Unit-cell assumptions
 - Outer surfaces with x=constant or y=constant are kept as planes with x=constant or y=constant, respectively
- Plane strain assumption
 - Outer surfaces with z=constant are kept as planes with z=constant.





FEM Compared to ND



- Previous residual stress measurements indicate a "stress-free" temperature of 650°C
- Material behavior of Kanthal from tensile test; Tungsten fibers assumed fully elastic
- Qualitative Agreement:
 - Residual strains, Yield point (region of co-deformation), Same ΔT for all volume fractions



FEM Compared to Macro Measurements



- Initial slope is similar for all
 - TRS induces micro-yielding that reduces apparent stiffness
 - At least measured neat and 30% behavior agrees with FEM
 - Waiting for independent tensile measurements on all volume fractions



Self-consistent model (SCM)

- Material parameters
 - Single crystal stiffnesses and coefficients of thermal expansion
 - Description of texture with discrete set of grain orientations
 - Crystal structure, slip (and twinning) systems
 - CRSS and hardening law
- Model Assumptions
 - Eshelby inclusion theory
 - HEM properties equal to weighted average of the grains



- Output
 - Direct comparison with neutron diffraction measurements
 - Averages over grains sets representing reflections



Single Crystal Elastic Constants



- Assumption of calculation of macroscopic moduli from single crystal values
 - Reuss-Voigt
 - Bollerath, Hauk & Müller
 - de Wit (based on Eshelby theory)
- Crystal symmetry
- Slopes gives diffraction elastic constants
 - $\mathsf{E}_{\mathsf{hkl}}$ and $\mathbf{v}_{\mathsf{hkl}}$

- Single crystal elastic stiffnesses from neutron diffraction data
 - T. Gnäupel-Herold, P.C. Brand and H.J. Prask, J. Appl. Cryst., 1998, vol. 31, pp. 929-935



Polycrystal versus Continuum Constitutive Description



SCM Compared to ND



- Macroscopic stress/strain curve for monolithic Kanthal
 - Used to fit the macro result of the model to the measurements
 - Enables direct comparison on the micro level
- Different sets of active slip systems



SCM Compared to ND



- Variation of plastic anisotropy depending on active slip systems
- Best agreement with only one set of active systems is {321}<111>
- Parameter study
 - Could indicate relative level of activity on different slip systems



Conclusions

- Neutron diffraction measurements
 - Unique ability to measure *in-situ* phase strains in MMC's during loading
 - Directly applicable for model validation on a microstructural level
- FEM predictions show qualitative agreement with the measurements
 - Micro yielding in composites; residual strains
 - Model development
 - Unit cell assumptions; hexagonal, cubic, coaxial, multi fiber, ...
- SCM predictions show qualitative agreement with the measurements
 - Monolithic Kanthal only
 - Quantitative agreement in the elastic region
 - Plastic anisotropy depends on set(s) of active slip systems

