



DAKOTA/UQ: A Toolkit For Uncertainty Quantification in a Multiphysics, Massively Parallel Computational Environment

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LANL Uncertainty Quantification Working Group

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Sandia is a multiprogram laboratory operated by Sandia Corporation, a Lockheed Martin Company, for the United States Department of Energy under contract DE-AC04-94AL85000.



Uncertainty Quantification



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Real Physical Systems:

- Display random and systematic variation- geometry, materials, boundary conditions, initial conditions, excitations
- Vary from one realization to the next
- Display behavior that cannot be precisely measured

Uncertainty occurs in various forms:

- Irreducible, variability, aleatoric
- Reducible, epistemic, subjective, model form uncertainty

Uncertainty Quantification



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Useful in:

- **Analysis and Design**

- To assess the reliability of physical systems.
- To establish designs that satisfy pre-established reliability requirements.
- To establish sensitivities to key uncertainties

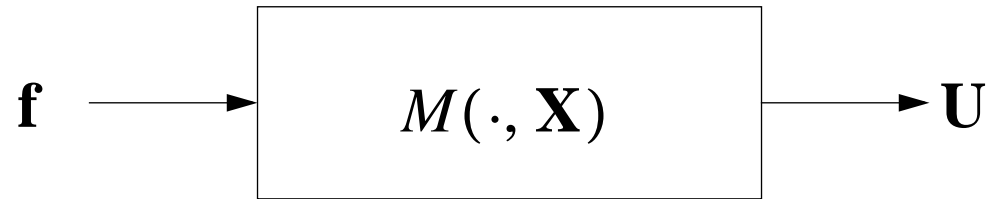
- **Model validation, certification, and accreditation**

- As defined in the DOE Defense Programs (DOE/DP) ASCI Program Plan, validation is the process of determining the degree to which a computer model is an accurate representation of the real world from the perspective of the *intended model applications*.
- Convey confidence in predictions to decision makers

Uncertainty Quantification: General Framework

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General Description:



\mathbf{X} : vector of uncertain parameters

M : a deterministic mapping

\mathbf{U} : output(s) of system

\mathbf{f} : input(s) to system

Statistical Approach:

- Model components of \mathbf{x} as *Random Variables or Fields*, and f as (possibly) *Random External Input*
- Seek quantities such as $E[g(\mathbf{U})]$. However, what is actually obtained are *conditional* statistics $E[g(\mathbf{U})|M]$.

Probabilistic/Statistical Approach: Essential Elements of a Statistical Approach:

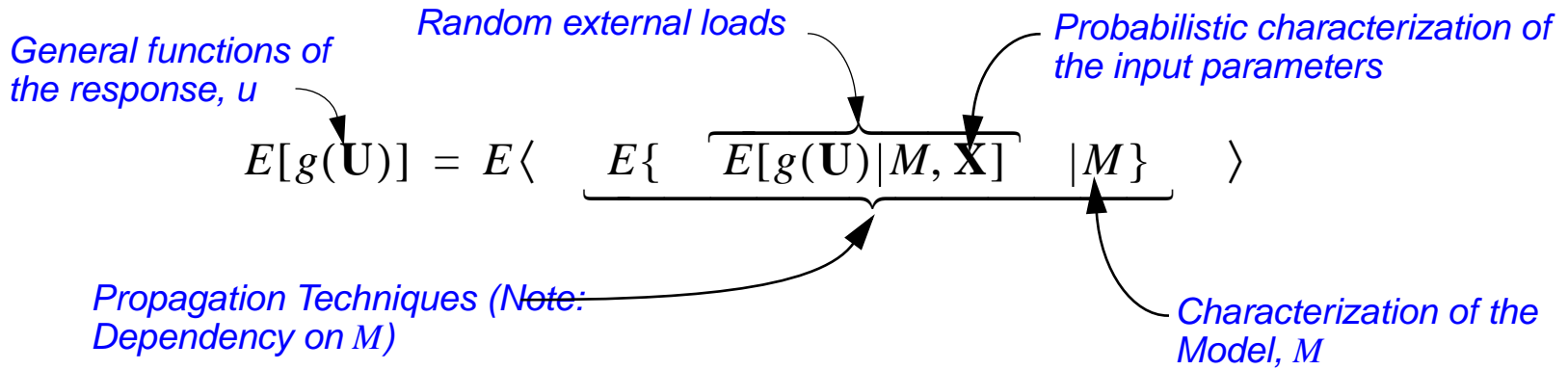


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Conclusion: Need a Generalized Outlook.

Essential Elements of a Statistical Approach:

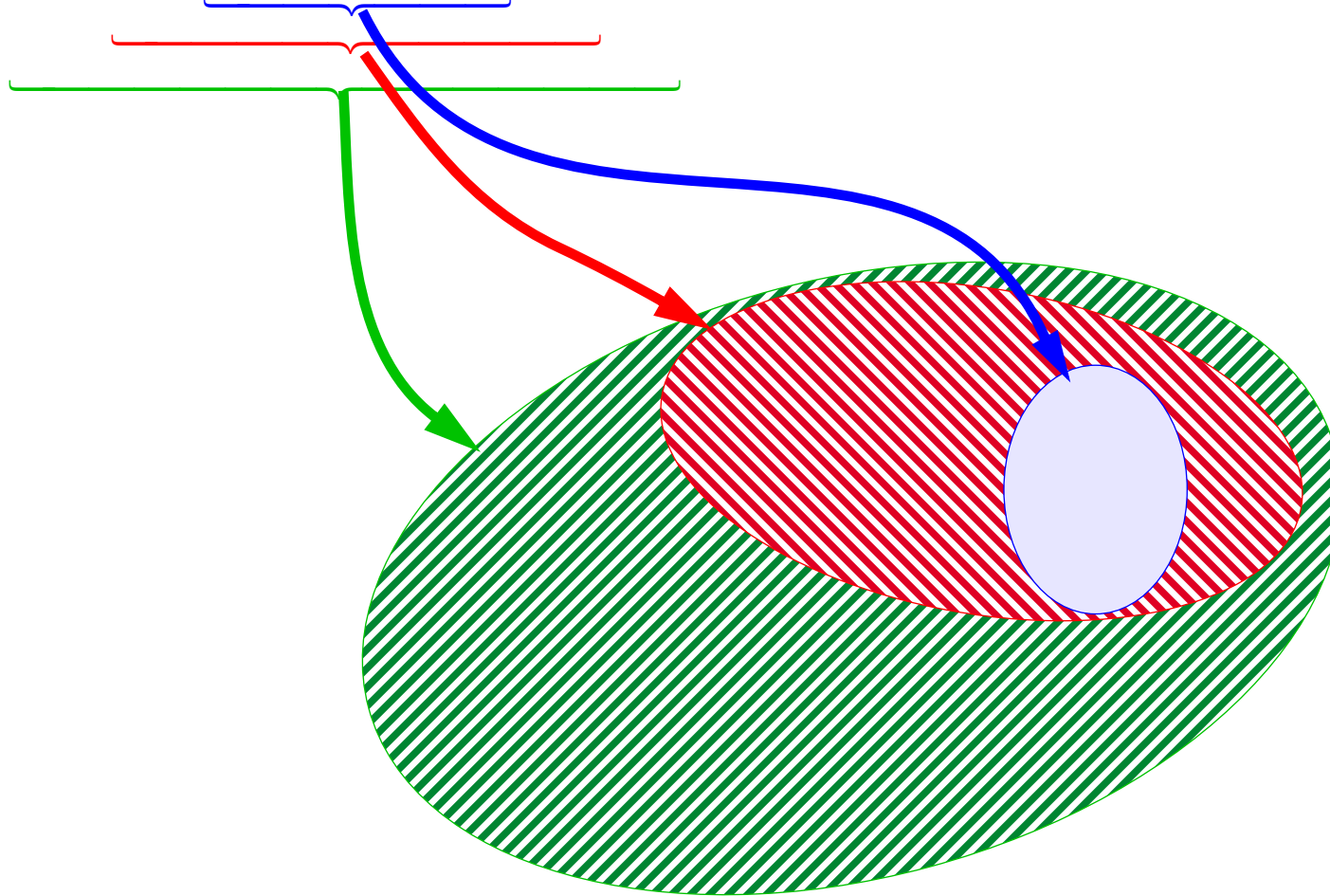
- **Random External Inputs**
- **Propagation Techniques**
 - Analytical Reliability Methods; Sampling; Response Surface Approximations; Stochastic Finite Element Methods.
- **Characterization of Models**
 - Verification and Validation.



Anatomy of Global Uncertainty

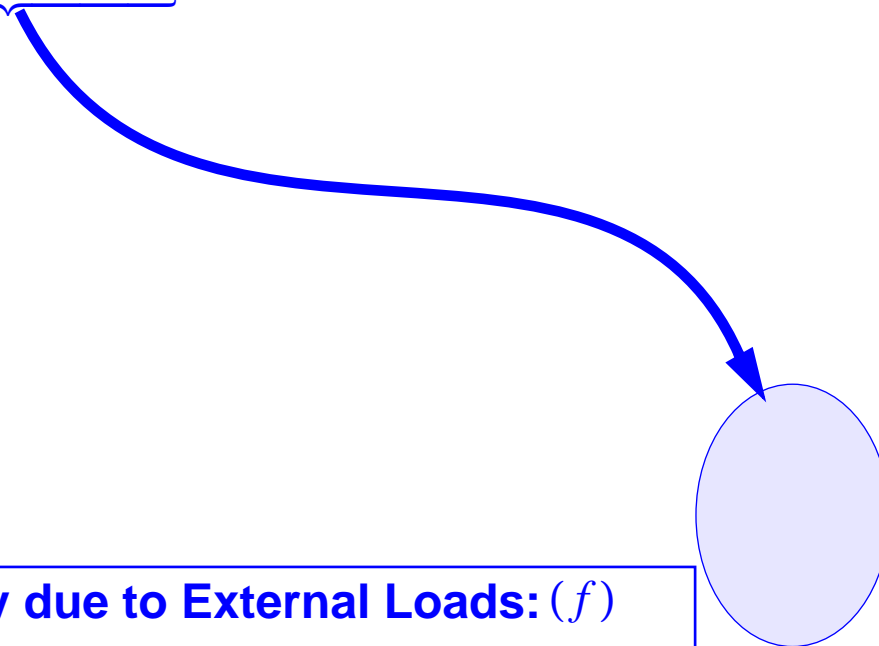
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$$E \langle E \{ \underbrace{E[g(\mathbf{U}) | M, \mathbf{X}] | M}_{\text{red}} \} \rangle = E[g(\mathbf{U})]$$



Anatomy of Global Uncertainty

$$E[g(\mathbf{U})|M, \mathbf{X}]$$



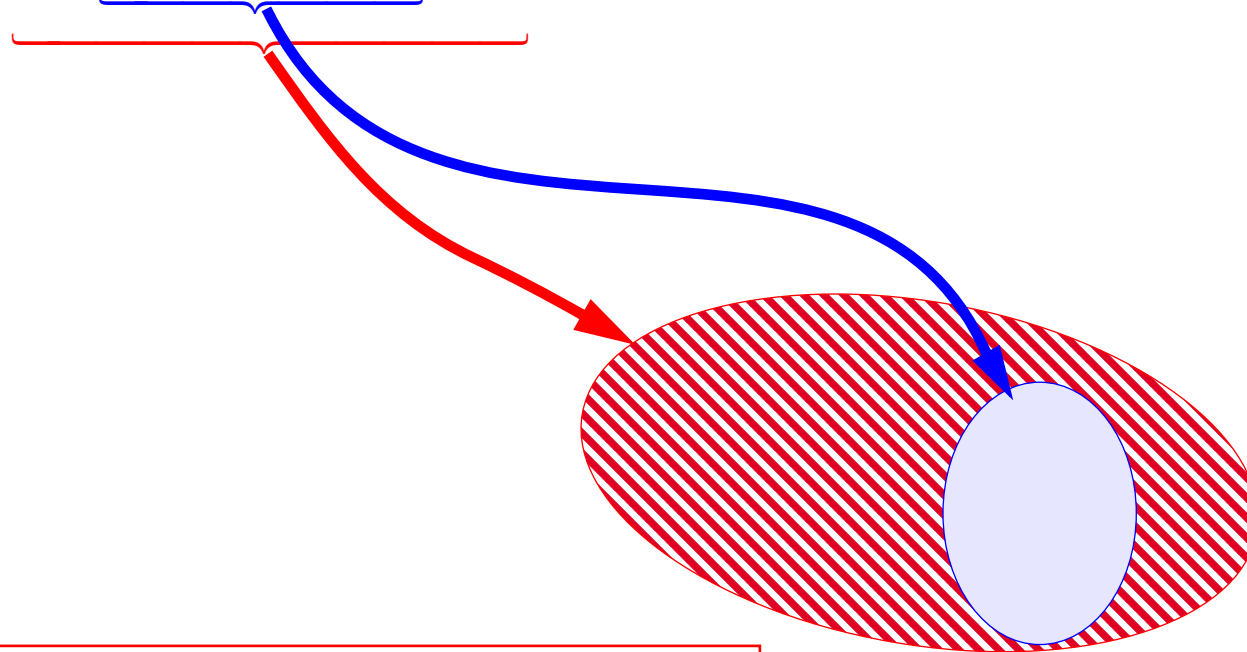
Uncertainty due to External Loads: (f)

- Random Vibration
- Earthquake Engineering
- Ocean Engineering
- Weapons Applications:
 - Launch Shocks/Re-entry Loads,
 - Penetration Loads,
 - Hostile Environments

Anatomy of Global Uncertainty

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$$E\{ \underbrace{E[g(U)|M, X]}_{\text{red bracket}} | M \}$$



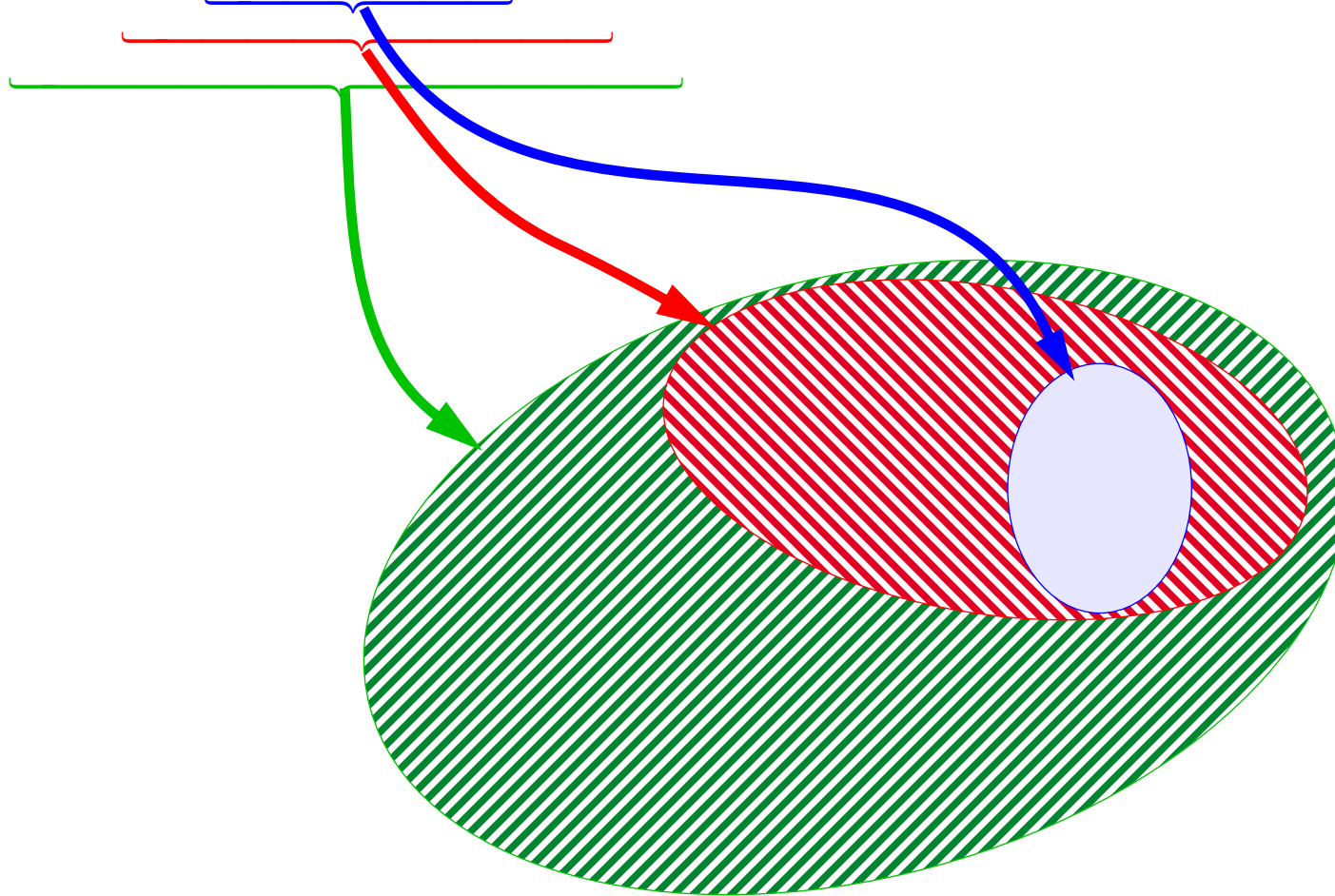
Uncertainty Propagation: (X)

- Effects of parametric uncertainty:
Intrinsic variabilities, Tolerances,
Lack of repeatability

Anatomy of Global Uncertainty

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$$E\langle E\{ \underbrace{E[g(\mathbf{U})|M, \mathbf{X}] | M}_{\text{red}} \} \rangle = E[g(\mathbf{U})]$$



Uncertainty Quantification at Sandia-NM



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- **DAKOTA (Design Analysis Kit for OpTimizAion)/UQ**
 - Framework for multi-level, parallel computation: ASCI-level problems, optimization, nondeterministic analysis, response surface approximation, design of experiments, optimization under uncertainty

- **Polynomial Chaos and Stochastic Finite Elements**
 - Analysis of response of stochastic systems

- **Epistemic Uncertainty**
 - Non-Probabilistic Approach, Probabilistic Approach, Model Uncertainty

- **Sensitivity Analysis**

Objectives of Toolkit



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Provide uncertainty quantification tools to the analyst community in a unified framework to be used in the design and certification processes.

- **Discipline independent**
- **ASCI (Accelerated Strategic Computing Initiative)-scale problems**
- **Minimize number of function evaluations**
- **Flexibility in uncertainty model**

Why tie UQ tools to the DAKOTA framework?

- **Existing, proven software framework**
- **Successfully linked with over 20 application codes**
- **Multilevel parallelism**
- **Extensive optimization algorithm library (gradient and non-gradient)**
- **Extensive selection of approximation strategies**

DAKOTA toolkit

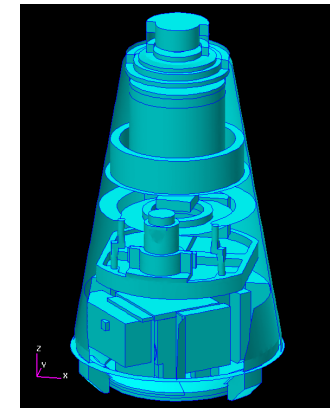
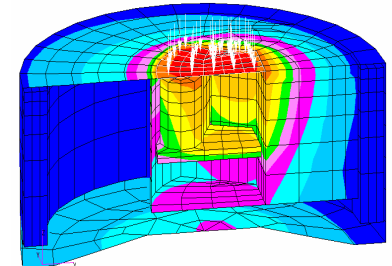
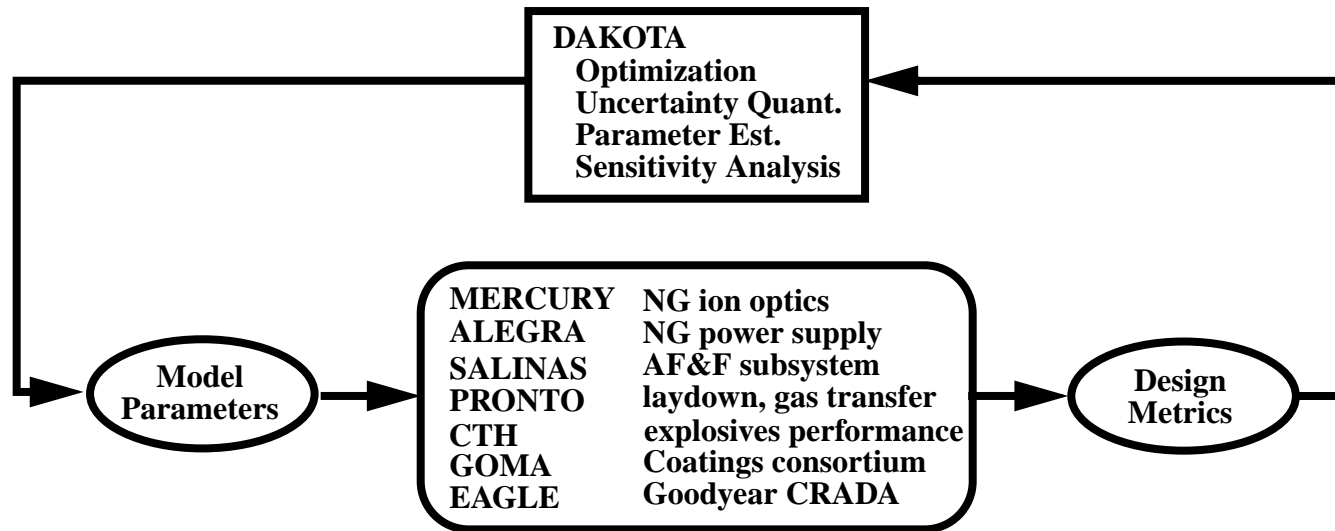
Design optimization of engineering applications



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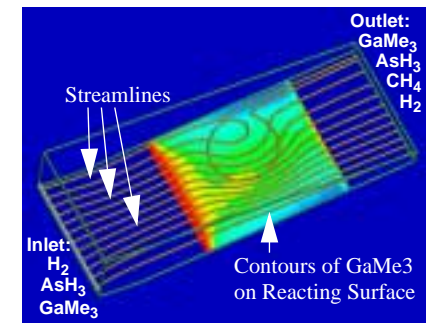
Answer fundamental engineering questions:

- What is the best design?
- How safe is it?
- How much confidence in my answer



Additional motivations:

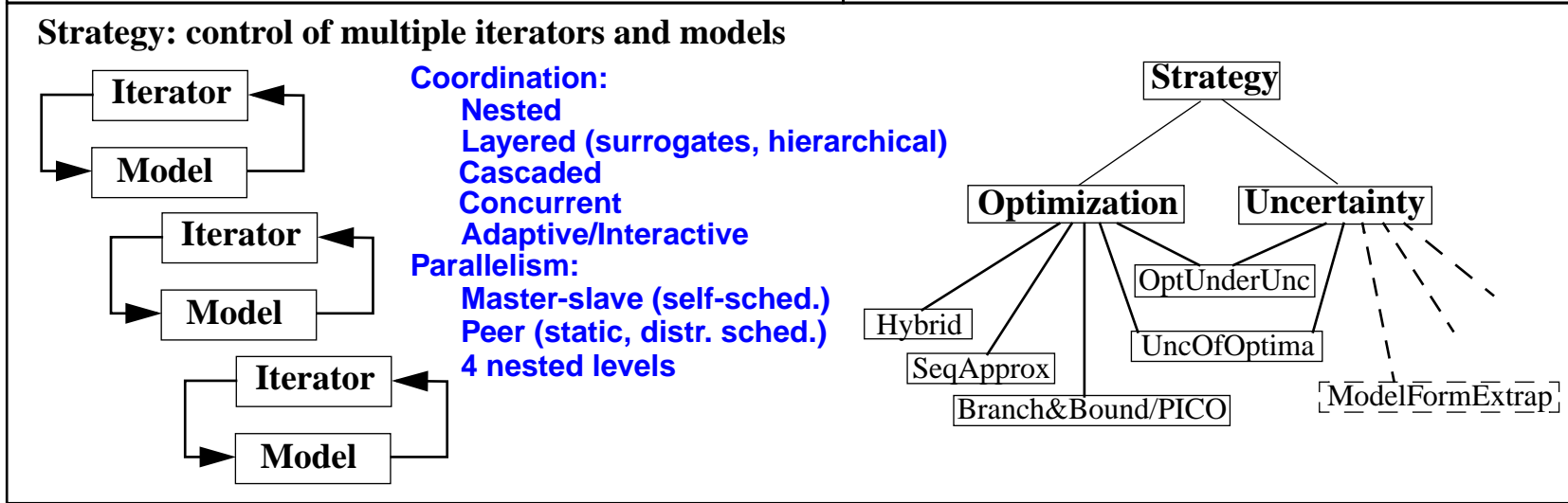
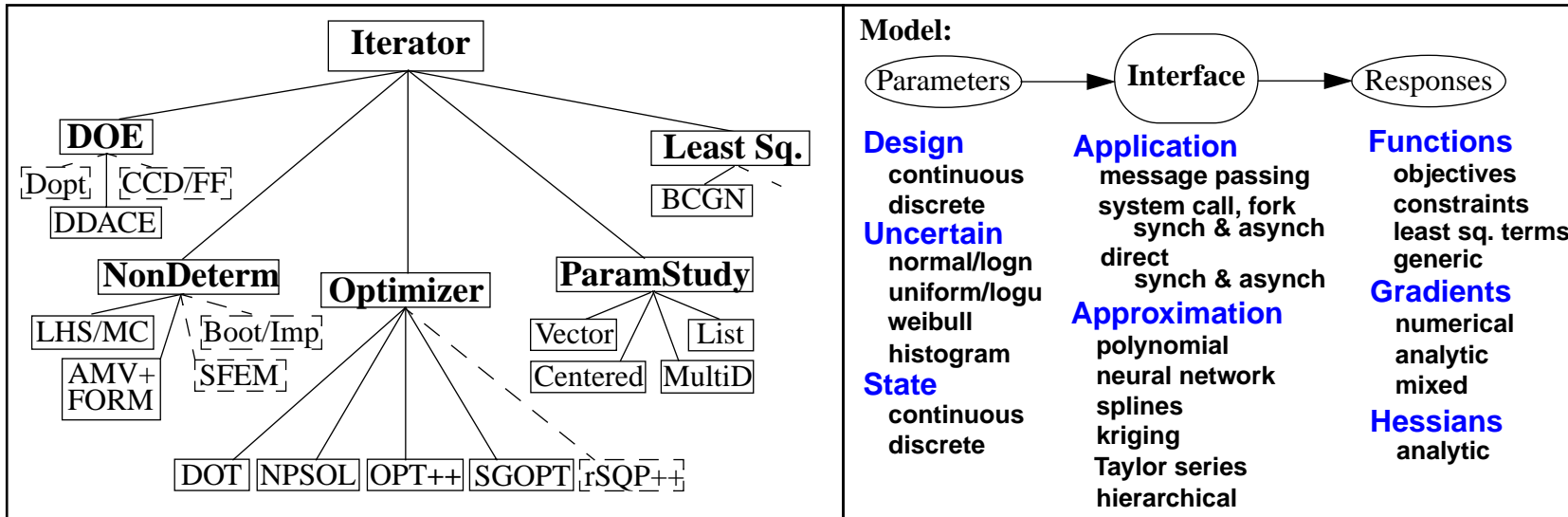
- Reuse tools and interfaces
- Leverage optimization, UQ, *et al.*
- Nonconvex, nonsmooth design spaces → state-of-the-art methodologies
- ASCI-scale applications and architectures → scalable parallelism
- Be a pathfinder in enabling M&S-based culture change at Sandia



Overview of DAKOTA framework



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Optimization/UQ Projects



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DAKOTA project (optimization with engineering simulations):

Sandia manager - David Womble, 9211, dewombl@cs.sandia.gov, 845-7471

PI - Mike Eldred, 9211, mseldre@sandia.gov, 844-6479

Team members - Tony Giunta, Bill Hart, Bart van Bloemen Waanders

<http://endo.sandia.gov/DAKOTA/>

DAKOTA/UQ project (analytic reliability, sampling, and SFE UQ library):

Sandia manager - Martin Pilch, 9133, mpilch@sandia.gov, 845-3047

PI - Steve Wojtkiewicz, 9124, sfwojtk@sandia.gov, 284-5482

Team members - Mike Eldred, Rich Field, John Red-Horse, Angel Urbina

SGOPT project (stochastic global optimization):

Sandia manager - David Womble, 9211, dewombl@cs.sandia.gov, 845-7471

PI - Bill Hart, 9211, wehart@cs.sandia.gov, 844-2217

<http://www.cs.sandia.gov/~wehart/main.html>

PICO project (mixed integer programming, scheduling and logistics):

Sandia manager - David Womble, 9211, dewombl@cs.sandia.gov, 845-7471

PI - Cindy Phillips, 9211, caphill@cs.sandia.gov, 845-7296

Team members - Bob Carr, Jonathan Eckstein (Rutgers), Bill Hart, Vitus Leung

<http://www.cs.sandia.gov/~caphill/proj/pico.html>

OPT++/DDACE/APPS/IDEA projects (NLP, sampling, & pattern search libraries):

Sandia manager - Chuck Hartwig(acting), 8950, hartwi@ca.sandia.gov

PI - Juan Meza, 8950, meza@ca.sandia.gov, 294-2425

Team members - Paul Boggs, Patty Hough, Tamara Kolda, Leslea Lehoucq,
Kevin Long, Monica Martinez-Canales, and Pam Williams

<http://csmr.ca.sandia.gov/~meza/research.html>

Current Dakota/UQ Capabilities



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Sampling Techniques:

- **Random Sampling (Monte Carlo)**
- **Stratified Sampling (LHS (Latin Hypercube Sampling))**

Analytical Reliability Techniques:

- **Mean Value (MV), Advanced Mean Value (AMV/AMV+)**
- **FORM (First Order Reliability Method)/SORM (Second Order Reliability Method)**

Robustness Analysis

Stochastic Finite Element/ Polynomial Chaos Expansions

Response Surface Approximations:

- **Application of UQ tools to a surrogate function to minimize computational expense.**

Sampling Techniques



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Monte Carlo-Style (Sampling-based) Analysis:

- **General, simple to implement and robust to size and discipline of problem being investigated**
- **Easily wrapped around current deterministic analysis capabilities**
- **Computationally expensive (many function evaluations)**
- **Two current options:**
 - Traditional Monte Carlo
 - Latin Hypercube Sampling
- **Under investigation:**
 - Bootstrap Sampling
 - Importance Sampling Techniques
 - Quasi-Monte Carlo Simulation
 - Markov Chain Monte Carlo

Overview of Analytically Based Reliability Methods



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- Involve a transformation to unit variance, uncorrelated normal random variable space.
- Nataf Transformation used in DAKOTA/UQ.
- MV, AMV/AMV+, FORM all solve a constrained optimization problem where the objective function is always this minimum distance function with the constraint function depending on the method.
- MV and AMV/AMV+ work in the original random variable space.
- FORM/SORM work in the transformed space.
- Equivalent to Polynomial Response Surface Techniques about an “optimally” selected expansion point

Probabilistic Robustness Analysis



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- “Given the bounds on the input parameters, what range of output function is possible?”
- Pose two global optimization problems:

$$g_{upper} = \max_{\mathbf{x}} g(M(f, \mathbf{x}))$$

$$g_{lower} = \min_{\mathbf{x}} g(M(f, \mathbf{x}))$$

such that

$$(x_i)_L \leq x_i \leq (x_i)_U \quad \forall \quad i = 1 \dots N$$

where N is the size of uncertain input vector, denote \mathbf{X}_L and \mathbf{X}_U its lower and upper bounds, respectively.

Probabilistic Robustness Analysis



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Answer:

$$g(\mathbf{u}) \in [g_{lower}, g_{upper}]$$

- Recently extended to mixed case of intervals and random variables of unknown dependence (to appear in Wojtkiewicz, AIAA SDM 2002)

SFEM/Polynomial Chaos Techniques



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- **Approximation of full stochastic representation**
- **Optimal approximation in inner product spaces, L_2 space of random variables.**
- **Represents a more general alternative to the Rosenblatt transformation**
 - avoid assuming full distribution when faced with limited input data
- **Estimating coefficients is the key issue**
 - requires realizations of the function it replaces
- **Convergence issues**
 - are there sufficient samples to compute coefficients?
 - possibility of non-physical realizations
 - mean square convergence

SFEM/Polynomial Chaos Techniques



- Consider PCE of general random process, u

$$u(x; \Phi) \approx u(x; \Phi)^{(P)} \equiv \sum_{i=0}^P u_i(x) \Gamma_i(\underline{\xi}), \text{ where } P = \sum_{s=1}^q \frac{1}{s!} \left\{ \prod_{r=0}^{s-1} (m+r) \right\}$$

– q th order polynomial in $\underline{\xi}$, where $\underline{\xi} = [\xi_1 \ \xi_2 \ \dots \ \xi_m]^T$

– function of m underlying random variables

- Solve for the Fourier coefficients, $u_i(x)$

$$u_i(x) = \frac{\langle u(x, h[\underline{\xi}]) \Gamma_i(\underline{\xi}) \rangle}{\langle \Gamma_i^2(\underline{\xi}) \rangle} = \frac{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \dots \int_{-\infty}^{\infty} u(x, h[\underline{\xi}]) \Gamma_i(\underline{\xi}) f_{\underline{\xi}}(\underline{\xi}) d\underline{\xi}}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \dots \int_{-\infty}^{\infty} \Gamma_i^2(\underline{\xi}) f_{\underline{\xi}}(\underline{\xi}) d\underline{\xi}} = \frac{n_i(x)}{\delta_i(x)}$$

$\delta_i(x)$ can be solved in closed-form

Epistemic Uncertainty



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- Epistemic Uncertainty results from a lack of information.
- Epistemic Uncertainty manifests itself in several ways
 - Uncertainty in parameters for which statistically significant databases do not exist
 - The form of the model is not known exactly

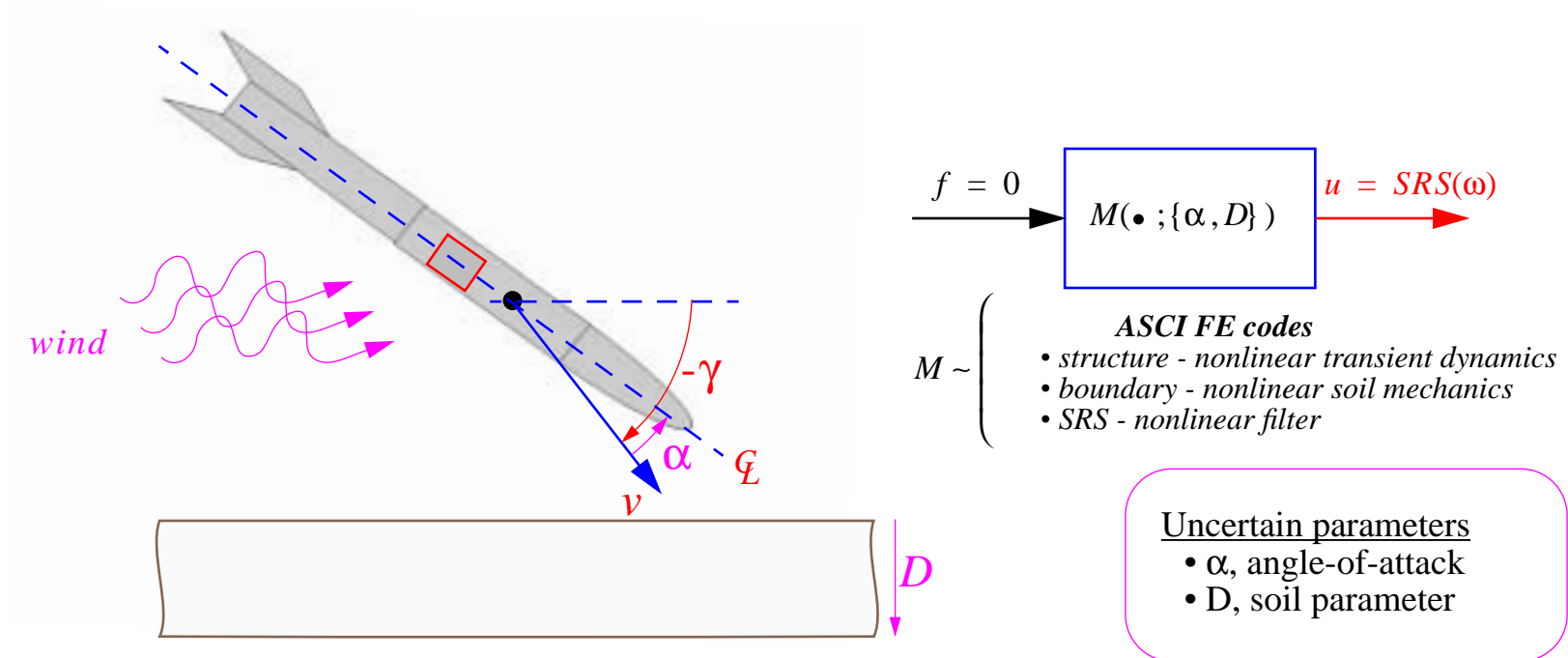
Non-Probabilistic Approach

- Variety of approaches investigated:
 - Interval analysis
 - Possibility Theory
 - Evidence Theory (Dempster-Shafer)
 - Imprecise Probability
 - Probability Bounds
 - Interval-valued Probability Distributions
 - Convex Sets of Probability Distributions

The Penetrator Problem

- Problem statement

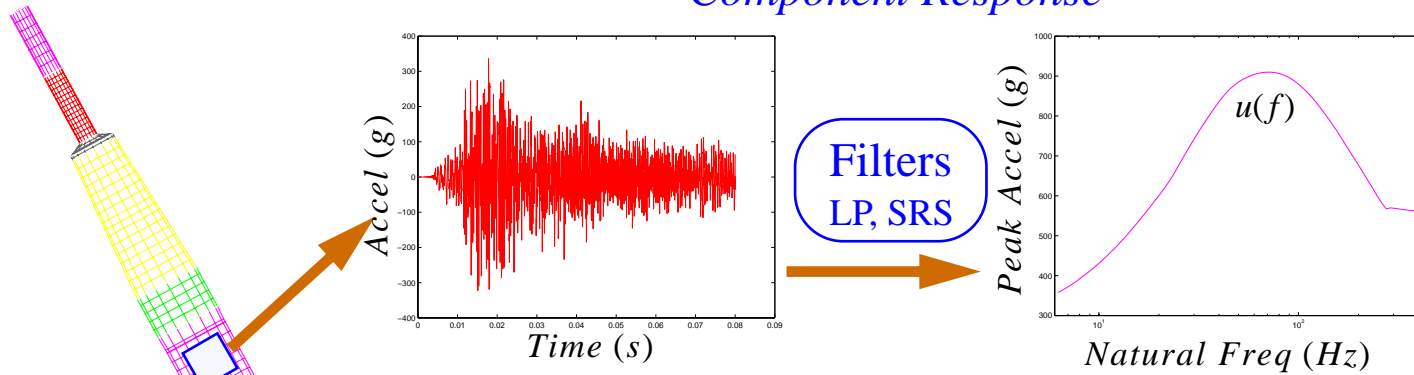
–During the penetration event, predict the probability of component failure, P_f



–Consider a nonlinear, full-body, 3D, coupled-physics simulation with simplified probabilistic properties.

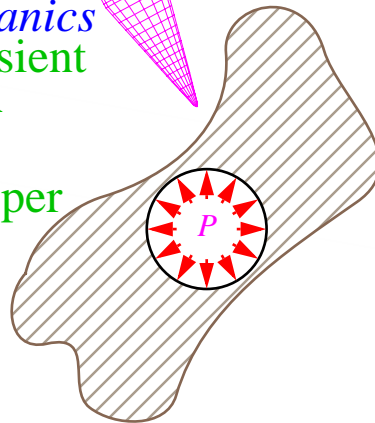
The model, M : a complex, cascaded system

Component Response



Structural Mechanics

- ✓ Nonlinear transient dynamics FEA
- ✓ 50,000 DOF
- ✓ 33 CPU hours per simulation

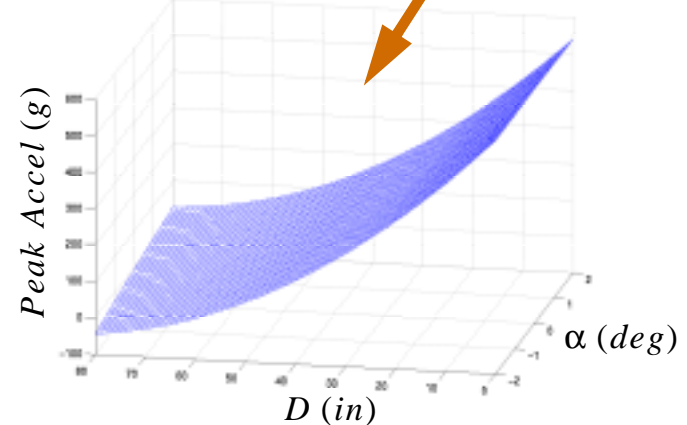


Soil Mechanics

- ✓ Spherical cavity expansion
- ✓ Loads couple with mechanics simulation

Approximate RS Models

- ✓ Performed simultaneously on network of Sun Ultra IIs
- ✓ 49 total runs performed



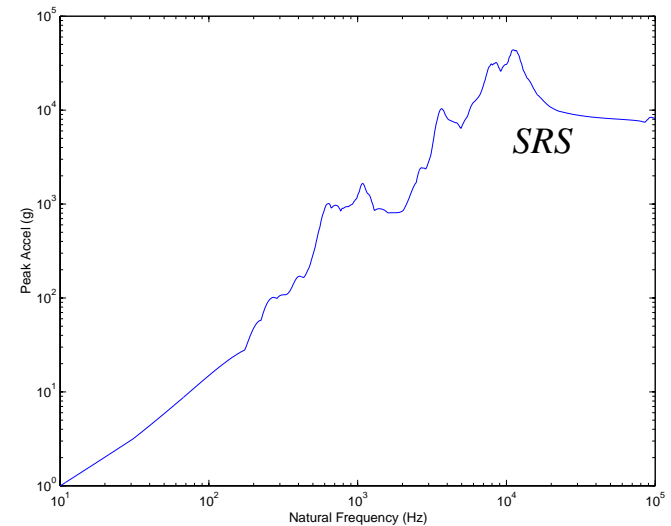
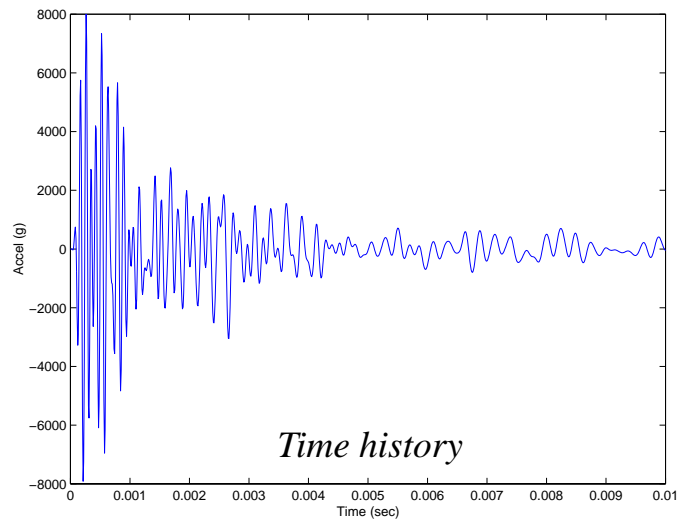
Overview of the Shock Response Spectrum (SRS)



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Why use SRS?

- measure of shock severity; indicative of shock damage potential
- frequency-domain representation of shock response
- long history of use in weapon design; test-based spec
- used for component qualification - compare to SRS_{ref}



UQ analysis of Penetrator System



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- **Two design variables, \mathbf{X} :**

- α , angle of attack is a normal random variable with mean 1 and standard deviation of 1.
- D , soil depth is a lognormal random variable with mean 25 and standard deviation 16.

$$\bar{u} = \min_i (SRS_{ref}(f_i) - SRS(f_i))$$

$$Z = g(\bar{U}) = I(\bar{U})$$

$$P_f = P(Z \leq 0) = 1 - E[g(\bar{U})]$$

- **Using the results from simulations, build a approximate model**

(response surface approximation) for \bar{u} .

UQ analysis of Penetrator System



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- Apply MC/LHS to these surrogate models to evaluate $F_Z(0)$:

$$N_s = 1 \times 10^4 \text{ and } N_s = 5 \times 10^6$$

Response Surface Approximation Method	<i>MC</i>	<i>LHS</i>
Kriging	0.02000/0.02300	0.02000/0.02400
Splines	0.06900/0.06781	0.06720/0.06767
Neural Net	0.05024/0.05588	0.05500/0.05581
Quadratic Polynomial	0.04960/0.05077	0.05070/0.05071

Summary



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Current Capabilities

Analytical Reliability Techniques:

- MV, AMV, AMV+, FORM/SORM

Sampling techniques:

- Pure Random Sampling (Monte Carlo)
- Stratified Sampling (LHS)

Probabilistic Robustness Analysis

Polynomial Chaos Expansions/Stochastic Finite Element Techniques

Future Capabilities:

Enhanced sampling methods:

- Importance Sampling, Bootstrap Sampling,
Quasi-Monte Carlo Sampling, Markov Chain Monte Carlo Sampling

Non-traditional uncertainty methodologies